

OPTICAL COMMUNICATIONS SUMMARY OF SOME USEFUL FORMULAE

General

$$\begin{aligned}\Delta(\tau/L)_{\text{dis}} &= -(M + M_g)\Delta\lambda \\ f_{3dB}(\text{opt.}) \times L &= \frac{0.5}{\Delta(\tau/L)} \\ f_{3dB}(\text{elec.}) \times L &= \frac{0.35}{\Delta(\tau/L)} \\ R_{RZ} \times L &= \frac{0.35}{\Delta(\tau/L)} \\ R_{NRZ} \times L &= \frac{0.7}{\Delta(\tau/L)}\end{aligned}$$

Resonant Cavities

$$\Delta f_c = \frac{c}{2Ln}$$

Optics

$$\begin{aligned}R(\text{normal incidence}) &= \left(\frac{n_1 - n_2}{n_1 + n_2} \right)^2 \\ \sin \theta_c &= \frac{n_2}{n_1}\end{aligned}$$

Optical Fibres

Step Index:

$$\begin{aligned}\Delta &= \frac{n_1 - n_2}{n_1} \\ \text{NA} &= \sqrt{n_1^2 - n_2^2} \\ \Delta(\tau/L)_{\text{mod}} &= \frac{n_1 \Delta}{c} \\ \text{Single mode: } a/\lambda_0 &< \frac{2.405}{2\pi \cdot \text{NA}}\end{aligned}$$

Graded Index (Parabolic Profile):

$$\begin{aligned}\Delta &= \frac{n_1^2 - n_2^2}{2n_1^2} \\ n(r) &= n_1 \sqrt{1 - 2(r/a)^2 \Delta} \text{ for } r \leq a \\ \text{NA} &= n_1 \sqrt{2\Delta} \sqrt{1 - (r/a)^2} \\ \Delta(\tau/L)_{\text{mod}} &= \frac{n_1 \Delta^2}{2c} \\ n_{\text{eff}} &= n_1 - (p + q + 1) \frac{\sqrt{2\Delta}}{k_0 a}\end{aligned}$$

Source Bandwidth

$$\begin{aligned}P_{SP} &= \frac{a_1 I_{SP}}{\sqrt{1 + \omega^2 \tau^2}} \\f_{3dB} &= \frac{1}{2\pi\tau} \\t_r &= \frac{0.35}{f_{3dB}}\end{aligned}$$

Source Coupling

For a source with pattern $\cos^m \theta$:

$$\begin{aligned}\eta_{\text{SI}} &= 1 - [1 - (\text{NA})^2]^{(m+1)/2} \text{ to SI Fibre} \\ \eta_{\text{GRIN}} &= \eta_{\text{SI}} \left\{ 1 - 0.5 \left(\frac{a_e}{a_f} \right)^2 \right\} \text{ to GRIN Fibre where } a_e \leq a_f\end{aligned}$$

Optical Detectors

$$\begin{aligned}\rho &= i/P = \frac{M\eta e\lambda}{hc} \\f_{3dB} &= \frac{0.35}{t_r} \\t_r &= 2.19 R_L C_d\end{aligned}$$

Analogue Modulation

AM/IM:

$$\begin{aligned}i &= I_0 + I_s(1 + m \cos \omega_m t) \cos \omega_{sc} t \\P &= P_0 + P_s(1 + m \cos \omega_m t) \cos \omega_{sc} t\end{aligned}$$

FM/IM:

$$\begin{aligned}i &= I_0 + I_s \cos(\omega_{sc} t + \beta \sin \omega_m t) \\P &= P_0 + P_s \cos(\omega_{sc} t + \beta \sin \omega_m t) \\B &= \frac{\omega_m}{\pi}(1 + \beta)\end{aligned}$$

LED Operating Characteristics

$$\begin{aligned}\lambda_0 &= \frac{1.24}{W_g(\text{eV})} \\P &= \eta i W_g(\text{eV}) \\P_s &= \frac{a_1 I_s}{\sqrt{1 + \omega^2 \tau^2}}\end{aligned}$$

Harmonic Distortion

$$P = P_{dc} + a_1 i_s + a_2 i_s^2 + \dots$$

$$\text{THD} = 0.25 \left(\frac{a_2 I}{a_1} \right)^2 \quad \text{for } i_s = I \sin \omega t$$

Receiver Design

General Signal to Noise Ratio:

$$S/N = \frac{(m^2/2)(M\rho P)^2 R_L}{M^n 2eR_L \Delta f (I_D + \rho P) + 4kT \Delta f F}$$

Thermal noise limited probability of error:

$$P_e = \frac{1}{2} - \frac{1}{2} \text{erf} \left(0.354 \sqrt{S/N} \right)$$

$$\text{erf}(x) \approx 1 - \frac{e^{-x^2}}{\sqrt{\pi}x} \quad \text{for } x \geq 3$$

Peak S/N (with threshold set at $0.5i_s$) for specified bit error rates.

P_s	S/N
10^{-4}	17.4dB
10^{-6}	19.5dB
10^{-9}	21.5dB

Quantum noise limited probability of error:

$$P_e = e^{-n_s}$$

$$n_s = \frac{\eta P_T}{hf}$$

Heterodyne Receivers

$$i_{dc} = \frac{\eta e}{hf} (P_L + P_S)$$

$$i_{IF} = \frac{2\eta e}{hf} \sqrt{P_L P_S} \cos [\omega_{IF} t - \theta(t)]$$

$$S/N = \frac{2 (\eta e/hf)^2 R_L P_S P_L}{2eR_L \Delta f [I_D + (\eta e P_L/hf)(1 + P_S/P_L)] + 4kT \Delta f}$$

Some Physical Constants

Speed of Light in Free Space	$c = 3 \times 10^8 \text{ m/s}$
Boltzmann's Constant	$k = 1.38 \times 10^{-23} \text{ J/K}$
Planck's Constant	$h = 6.626 \times 10^{-34} \text{ Js}$
Electron Charge	$e = 1.6 \times 10^{-19} \text{ C}$